

11. References

1. Abo-Zena, A. N , 1977, Radiation from a finite cylindrical explosive source: *Geophysics*, **42**, 7, p. 1384-1393.
2. Abramovitz, M.and Stegun, I. A., (Editors), 1965, *Handbook of Mathematical Functions*, Dover, New York.
3. Baron, M. L.and Matthews, A.T., 1961, Diffraction of a pressure wave by a cylindrical cavity in an elastic medium: *J. App. Mech.*, Trans. ASME, **28**, p.347 - 354
4. Baron, M. L. and Parnes, R., 1962, Displacements and velocities produced by the diffraction of a pressure wave by a cavity in an elastic medium: *J. App. Mech.*, Trans. ASME, June 1962,
5. Bathe, K. J., 1975, ADINA - A Finite Element Program for Automatic Dynamic Incremental Non-linear Analysis: Report No. 82448-1, M.I.T. Mech. Eng. Dept., Acoustics and Vibration Lab. Massachusetts Inst. of Tech., (1978 revision).
6. Bathe, K. J., and Wilson E. L., 1976, *Numerical Methods in Finite Element Analysis*: Prentice Hall, New Jersey.
7. Belytscho, T. and Mullen, R., 1977, On dispersive properties of finite element solutions: *Modern Problems in Elastic Wave Propagation*: Editors, Miklowitz, J. and Achenbach, J. D., Wiley, New York, p.67-82.

8. Blair, D. P., 1975. The solid tidal strain tensor: Ph. D. thesis, Dept. of Geophysics, University of New England, Armidale, N.S.W.
9. Blair, D. P., 1982, Dynamic modelling of in-hole mounts for seismic detectors: *Geophys. J. R. astr. Soc.*, 69, p. 803 - 817.
10. Blair, D. P., 1984, Rise-times of attenuated seismic pulses detected in both empty and fluid-filled boreholes: *Geophysics*, 49, 4, p. 398-410.
11. Blair, D. P., Siggins, A. F., and Wold, M. B., 1984, Stress sensitivity of pulse velocity and rise-time in a rock-like material: *Int. J. Rock Mech. Min. Sci. & Geomech. Abstr.* , 21, p. 219-221.
12. Bruel and Kjaer, 1974, *Accelerometers. Instructions and Applications.*
13. Buchwald, V. T., 1978, The diffraction of elastic waves by small cylindrical cavities: *J. Austral. Math. Soc.* , 20, Series B, p. 495-507.
14. Cheng, S. L. and Jananashi, A., 1967, On dynamic stress concentration around a discontinuity: *J. Appl. Mech.*, Trans., ASME, June 1967, p. 385-389.
15. Cook, E. G. and Valkenburg, H. E., 1954, Surface waves at ultrasonic frequencies: *ASTM Bull.* , 3, p. 81-84.
16. Dowding, C. H., 1978, Damage to rock tunnels from earthquake shaking: *J. Geotech. Eng. Div.*, GT2, Feb., p. 175-190.

17. Eason, G., 1973, Propagation of waves from spherical and cylindrical cavities: *ZAMP*, **14**, p.12.
18. El-Akily, N. and Datta, S. K., 1980, Response of a circular cylindrical shell to disturbances in a half-space: *Earthquake Eng. and Struct. Dynamics*, **8**, p. 469-477.
19. Gladwin, M. T. and Stacey, F.D., 1974, Ultrasonic pulse velocity as a rock stress sensor: *Tectonophysics*, **21**, p. 39-45.
20. Glass, C. E., 1974, Seismic considerations in siting large underground openings in rock: Ph. D. Thesis, University of California, Berkeley.
21. Greenfield, R. J., 1978, Seismic radiation from a point source on the surface of a cylindrical cavity: *Geophysics*, **43**, 6, p. 1071-1082.
22. Gupta, I. N., 1965, Note on the use of reciprocity theorem for obtaining radiation patterns: *Bull. Seismo. Soc. Am.*, **55**, 2, p. 277-281.
23. Heelan, A. P., 1953, Radiation from a cylindrical source of finite length: *Geophysics*, **18**, p. 685-696.
24. Knopoff, L. and Gangi, A. F., 1959, Seismic reciprocity: *Geophysics*, **XXIV**, 4, p. 681-691.
25. Lamb, H., 1904, On the propagation of tremors over the surface of an elastic solid: *Phil. Trans. Roy Soc., A*, **203**, p. 1-42.

26. Lee, M. W., 1986, Low-frequency radiation from point sources in a fluid-filled borehole: *Geophysics*, **51**, 9, p.1801-1807.
27. Lee, M. W., 1987, Particle displacements on the wall of a borehole from incident plane waves: *Geophysics* , **52**, 9, p. 1290-1296.
28. Lysmer, J.and Kuhlemeyer, R. L.,1969, Finite element model for infinite media: *Proc. ASCE, J. Eng. Mech. Div.*, August, p. 859-877.
29. Miklowitz, J., 1963, Pulse propagation in a viscoelastic solid with geometric dispersion: *Stress Waves in Anelastic Solids*, IUTAM Symposium. Editors, Kolsky H. and Prager W. Springer-Verlag, Berlin, p. 255-276.
30. Miklowitz, J., 1966, Scattering of a plane compressional pulse by a cylindrical cavity: *Int. Cong. Appl. Mech.*, Proceedings of the 11th, Munich, Germany, p. 469-483.
31. Miklowitz, J., 1980, *Elastic Waves and Waveguides*. (2nd Ed.) North-Holland, New York.
32. Mooney, H. M.,1974, Some numerical solutions for Lamb's problem: *Bull. Seis. Soc. Am.*, **64**, 2, p. 473-491.
33. Mow, C. C. and Mente, L. J. 1963, Dynamic stresses and displacements around cylindrical discontinuities due to plane harmonic shear waves: *J. Appl. Mech.*, Trans ASME., December 1963, p. 598-604.
34. NAG5, 1977, FORTRAN Library manual: Oxford Univ. Computer Library.

35. Nakano, H., 1928, Rayleigh waves in cylindrical coordinates: *The Geophysical Magazine* (Central Meteorological Observatory of Japan, Tokyo), 1, p. 1926 - 1928.
- 36 Newmark, N., M., 1959, A method of computation for structural dynamics: *A.S.C.E., J., Eng., Mech., Div.*, **85**, p. 67 - 94.
37. Nishimura, G. and Jimbo, Y., 1954, A dynamical problem of stress concentration. Stresses in the vicinity of a spherical matter included in an elastic solid under dynamical force: *J. Faculty of Eng., Univ. of Tokyo.*, **XXIV**, 3.
38. Oldham, R. D., 1900, On the propagation of earthquake motion to great distances: *Phil. Trans. Roy. Soc. A*, **194**, p. 135.
39. Pao, Y. H., 1962, Dynamical stress concentration in an elastic plate: *J. App. Mech.*, *Trans. ASME.*, **2**, p. 299-305.
40. Pao, Y.H.and Mow, C.C., 1962, Dynamical stress concentration in an elastic plate with a rigid circular inclusion: *Proc. 4th Int. Cong. of Appl. Mech.* June 1962, p. 335-345.
41. Pao, Y.H. and Mow, C.C., 1973, *Diffraction of Elastic Waves and Dynamic Stress Concentrations*., Crane, Russak and Co., New York, The Rand Corporation.
42. Pao, Y. H. and Mow, C. C., 1976, Theory of normal modes and ultrasonic spectral analysis of the scattering of waves in solids: *J. Acoust. Soc. Am.*, **59**, 5, p. 1046-1056.

43. Pao, Y.H. and Sachse, W., 1974, Interpretation of time records and power spectra of scattered ultra-sonic pulses in solids: *J. Acoust. Soc. Am.*, **56**, 5, p. 1478-1486.
44. Patterson, T. N. L., 1968, The optimum addition of points to quadrature formulae: *Mathematics of Computation*, **22**, p. 847-856.
45. Peck, J. C., 1965, Plane strain diffraction of transient elastic waves by a circular cavity: Ph.D. Thesis; Calif. Inst. of Tech.
46. Peck, J.C. and Miklowitz, J., 1969, Shadow-zone response in the diffraction of a plane compressional pulse by a circular cavity: *Int. J., Solids and Structures*, **5**, 5, p. 437-454.
47. Peralta, A., Carrier, G. F. and Mow, C. C., 1966, An approximate procedure for the solution of a class of transient-wave diffraction problems: *J. Appl. Mech.*, Trans ASME, March 1966, p. 168-172.
48. Perkins, B. R., 1980, FEVECO Version 3 - Post processing for finite element analysis. Tech. Report 117., CSIRO Division of Applied Geomechanics.
49. Rayleigh, Lord, 1885, Scientific Papers., **2**, p. 441 - 447.
50. Robinson, E. A. and Treitel, S., 1980, *Geophysical Signal Analysis*: Prentice-Hall, New Jersey.

51. Roever, W.L., Rosenbaum, J. H. and Vining T. F., 1974, Acoustic waves from an impulsive source in a fluid-filled borehole: *J. Acoust. Soc. Am.* , **55**, 6, p. 1144-1157.
52. Sachse, W., 1974, Ultra-sonic spectroscopy of a fluid-filled cavity in an elastic solid: Materials Science Centre Report 2175, Cornell Univ., Ithaca N.Y.
53. Selberg, H. L., 1952, Transient compressional waves from spherical and cylindrical cavities: *Arkiv fur Fysik.*, **5**, p. 97 - 108.
54. Setser, G. G., 1981, Fracture detection by circumferential propagation of acoustic energy: Petroleum Engineers, 56th Annual Fall Tech Conf., Paper SPE 10204.
55. Sezawa, K., 1927, Dispersion of elastic waves propagated on the surface of stratified bodies and curved surfaces: Univ. of Tokyo., *Bull. Earthquake Res. Inst.*, **3**, p. 1 - 18.
56. Shipley, S. A., Leistner, H. G. and Jones, R. E., 1967, Elastic wave propagation - a comparison between finite element predictions and exact solutions: Proc. Int. Symp. Wave Propagation and Dynamic Properties of Earthen Materials. Univ. of New Mexico, p. 509-519.
57. Siggins, A. F. and Enever J. R., 1979, A laboratory simulation of the influence of defects on the dynamic response of a rectangular mine opening: Proc. ISRM Cong. Rock Mech., Switzerland., p.293 -300.
58. Siggins, A. F. and Stokes, A. N., 1987, Circumferential propagation of elastic waves on boreholes and cylindrical cavities: *Geophysics*, **52**, 4, p. 514-529.

59. Siggins, A. F., 1982, A concentrated pressure pulse on a semi-infinite medium - A comparison between theory and dynamic finite element method: Proc. 4th Int. Conf. on Numerical Methods in Geomech., Edmonton, May 31- June 4, p. 449-457.
60. Siggins, A. F., 1983, Dynamic response of coal mine roof. Some observations at Wallsend Borehole Colliery: Geomechanics of Coal Mining Report No. 41, CSIRO Division of Geomechanics.
61. Siggins, A. F., 1986, Suggested methods for determining dynamic elastic properties of rock: Tech. Report 122, CSIRO Division of Geomechanics, p. 1-22.
62. Singleton, R. C., 1967, On computing the fast Fourier transform: *Commun., Assn. Comp. Math.*, **10**, p. 647-654.
63. Stokes, A. N., and Siggins, A. F., 1987, Complex singularities of the transfer function for cylindrical cavities in elastic media: *J. Appl. Mech.*, Trans. ASME., p. 974-976.
64. Su, W. H., Peng, S. S., Okubu, S. and Matsuki, K., 1983, Development of ultrasonic methods for measuring stresses at great depth: *Mining Sci. and Tech.*, **1**, p. 21-42.
65. Temme, N. M., 1975, On the numerical evaluation of the modified Bessel functions of the third kind: *J. Computational Phys.*, **19**, p. 324-337.

66. Thill, R. E. and Peng, S. S., 1974, Statistical comparisons of the pulse and resonance methods for determining elastic moduli: USBM, Report of Investigations 7831, p. 1-24.
67. Timoshenko, S. and Goodier, J. N., 1970, *Theory of Elasticity*., 3rd Edition, McGraw-Hill, New York.
68. Uberall, H., 1977, Modal and surface-wave resonances in acoustic wave scattering from elastic objects and elastic-wave scattering from cavities: *Modern Problems in Elastic Wave Propagation*: Editors, Miklowitz, J. and Achenbach, J. D., Wiley, New York, p. 239-263.
69. Valliapan, S. and Murti, V., 1984, Finite element constraints in the analysis of wave propagation problems: UNICIV Report No. R-218, Univ. of New South Wales.
70. Viktorov, I. A., 1958, Rayleigh type waves on a cylindrical surface: *Soviet Physics-Acoustics*, **4**, p. 131-136.
71. Vogel, C. B. and Heroltz, R. A., 1981, The CAD-circumferential device for well logging: *J. Petroleum Tech.*, October, p. 1985-1987.
72. White, J. E., 1960, Use of reciprocity for computation of low-frequency radiation patterns: *Geophysics*, **XXIV**,3, p. 613-624.
73. White, R. M., 1958, Elastic wave scattering at a cylindrical discontinuity in a solid: *J. Acoust. Soc. of Am.*, **30**, 8, p. 771-785.

74. White, W., Valliapan, S., and Lee, I. K., 1977, A unified boundary for finite dynamic models: *Proc. ASCE, J. Eng. Mech. Div.*, October, p. 949-964.
75. Ying, C.Zhang, S. and Wang, L., 1981, Study of the creeping waves around cylindrical cavities in a solid medium by the photoelastic technique: *Academia Sinica*, XXIV, 11, p.1509-1520.

Appendix 1. Computer program listings

88/07/25
14:54:02

NIKZX

1

```
PROGRAM NIKZX
C-----FINDS ZEROES IN Z-PLANE; POZ.FOR
      IMPLICIT COMPLEX (Z)
6      FORMAT (2F6.3,4F11.4,4F6.3)
      WRITE (1,100)
100  FORMAT ('ENTER R, ZP, ZDP, ZX')
7      READ (1,*) R, ZP, ZDP, ZX
      L=0
2      ZY=ZX*R
      CALL RAT (ZP, ZX, ZU, ZUD)
      CALL RAT (ZP, ZY, ZV, ZVD)
      ZPP=ZP*ZP
      ZYY=ZY*ZY
      ZUE=ZPP-ZX*ZX-ZU*ZU
      ZPQ=ZPP-1.
      ZVE=ZPP-ZYY-ZV*ZV
      ZM=ZV*ZU*ZPQ-(ZV+ZU)*ZYY/2. + ZPP*(ZYY-ZPP)+ZPP-ZYY*ZYY/4.
      ZME=ZPQ*(ZU*ZVE+ZV*ZUE)-ZYY*(ZV+ZU+.5*ZVE+.5*ZUE-2.*ZPP+ZYY)
      ZME=ZME/ZX
      ZMD=ZVD*(ZU*ZPQ-ZYY/2)+ZUD*(ZV*ZPQ-ZYY/2)+
      2.*ZP*(ZV*ZU+ZYY-2.*ZPQ-1.)
      ZDZ=-ZM/ZME
      ZX=ZX+ZDZ
      IF (CABS (ZDZ) .LE. .0008) GOTO 3
      GOTO 2
3      CONTINUE
      WRITE (6,6) ZP, ZX, ZME
      ZP=ZP+ZDP
      Z=Z2
      Z2=ZX-Z1
      Z1=ZX
      Z3=Z2-Z
      L=L+1
      IF (L.GT.2) ZX=Z1+Z2+Z3
      IF (REAL (ZX) .LE.0.) GOTO 7
      IF (CABS (ZP-5.) .LE.5.001) GOTO 2
      GOTO 7
      END
      SUBROUTINE RAT (ZP, ZX, ZF, ZFD)
      IMPLICIT COMPLEX (Z)
      ZI=(0.,1.)
      ZA=ZP+.5
      N=55
      ZN=1.+CSQRT (-2.*ZI*ZX/N)
      DO 1 J=1,N
          I=N+1-J
          ZZ=I-ZA+1.0E-09
          ZK=(I+1)*I/(ZA+I-1)/ZZ
          ZND=ZK/ZN/ZN*ZND-ZN/(ZA+I-1)+ZN/ZZ
1      ZN=(-2.*ZI*ZX+I+I)/(I+1)-1/ZN)*ZK
          ZF=-.5+ZI*ZX+1./ZN
          ZFD=-ZND/ZN/ZN
      END
```

88/07/25
14:55:43

LLD

1

```
PROGRAM LLD2
C   CALCULATES GREENS FUNCTIONS OF THETA FOR RANGE OF X.
C   THE PHASE RESPONSE IS UN-WRAPPED AND WRITTEN TO LLPH:TS
      IMPLICIT COMPLEX (Z)
      DIMENSION PHA(500)
      WRITE (1,200)
      READ (1,*) R,X,DX,XMAX
      WRITE (1,300)
      READ (1,*) NN, KK, RT
      OPEN (2, STATUS='UN', FILE='LOUT:TS')
      ZII=(0.,1.)
      J=0
      X=X-DX
2    X=X+DX
      J=J+1
4    Y=R*X
      YY=Y*Y
      XX=X*X
      RR=XX/YY
      DO 9 K=1, KK
      TH=3.14159*RT
      TH=TH*FLOAT(K/KK)
      CALL RAT(X, ZU)
      CALL RAT(Y, ZV)
      P=0.
      ZW=CEXP(TH*ZII)
      ZP=(.5,0.)
      ZSUM=P
      ZSUN=P
      DO 1 I=1, NN
      P=I-1
      PP=P*P
      ZQ=CONJG(ZP)
      ZT=ZV*ZU*(PP-1.)-(ZV+ZU)*YY/2. + PP*(YY-PP)+PP-YY*YY/4.
      ZMM=ZM
      ZM=(ZV*ZU+ZU*YY/2. -PP)/ZT
      ZSUM=ZSUM+ZM*(ZP+ZQ)
      ZNN=ZN
      ZN=ZII*P*(ZU*ZV+YY/2-PP)/ZT
      ZSUN=ZSUN+ZN*(ZP-ZQ)
      ZU=((P+1)*ZU+X*X-PP-P)/(P-ZU)
      IF (I.EQ.1) ZP=ZP+ZW
      ZP=ZP*ZW
1    ZV=((P+1)*ZV+YY-PP-P)/(P-ZV)
3    ZSUM=ZSUM+ZM*ZM*ZP/(ZMM-ZM*ZW)
      ZSUN=ZSUN+ZN*ZN*ZP/(ZNN-ZN*ZW)
      ZSUM=ZSUM+ZM*ZM/ZP/(ZMM-ZM/ZW)
      ZSUN=ZSUN-ZN*ZN/ZP/(ZNN-ZN*ZW)
      YPHA=AIMAG(ZSUM)/REAL(ZSUM)
      YPHA=ATAN(YPHA)
      PHA(J) = 57.295795*YPHA
      YMAG=CABS(ZSUM)
9    WRITE (2,100) TH, X, ZSUM, YMAG, YPHA
      IF (X.LE.XMAX) GOTO 2
      NP=INT(XMAX/DX)
      PI=180.
      TOL=0.4*PI
      K=2
19   CONTINUE
      DO 20 I=K, NP
      IF ((PHA(I-1)-PHA(I)).GT.TOL) GO TO 25
20   CONTINUE
25   K=I
      IF (K.GE.NP) GO TO 27
```

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14:55:43

LLD

2

```
DO 26 J=K, NP
PHA (J)=PHA (J) +PI
26 CONTINUE
IF (I.LT.NP) GO TO 19
27 CONTINUE
OPEN (3, STATUS='UN', FILE='LLPH:TS')
X=0.
DO 30 I=1, NP
X=X+DX
WRITE (3, 400) X, PHA (I)
30 CONTINUE
100 FORMAT (2F10.4, 4E12.5)
200 FORMAT ('ENTER R, X, DX, XMAX')
300 FORMAT ('ENTER NO.OF TERMS IN SUM, NO.OF INTERVALS 0-PI,
. FRACTION OF PI')
400 FORMAT (F10.2, 5X, E12.5)
END
SUBROUTINE RAT (Y, ZF)
IMPLICIT COMPLEX (Z)
ZI=(0., 1.)
Z1=(1., 0.)
Z0=(0., 0.)
ZA0=Z0
ZA1=.5
ZB0=Z1
ZB1=Y
DO 1 J=1, 150
ZC=Z1
ZD=.5*ZI*(J-.5)
DO2 K=1, 2
ZB2=ZB1*ZC+ZB0*ZD
ZA2=ZA1*ZC+ZA0*ZD
ZB0=ZB1/ZA1
ZA0=Z1
ZB1=ZB2/ZA1
ZA1=ZA2/ZA1
ZD=ZD+ZI*(.5)
2 ZC=Y
ZF=ZA2/ZB2
ZF=Y*(ZI-ZF)
C=CABS (ZF-ZF1)
IF (C.LT.1.0E-06) RETURN
1 ZF1=ZF
END
```

```

PROGRAM LLDISP(TAPE1,INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
DIMENSION X(200), SUMR(500), SUMS(500), SUMP(500), SUMT(500),
*ITIT(4)
COMMON /PART1/ R, TPT, VP, VS, PCA, PCB, AA, BB, CC
COMMON /PART2/ TIM(500), XLEN, NPLOTS, SCL
EXTERNAL FUN1
EXTERNAL FUN2
EXTERNAL FUN3
DATA ITIT /9HDISP.R X=,9HDISP.S X=,9HDISP.P X=,9HDISP.T X=/
XLEN = 0.0
NPLOTS = 0
READ (5,99999) NPTS1, NPTS2, SCL, VS, PCA, PCB, TSTEP, PTYP,
*NPRINT
IF(PTYP.EQ.2H )PTYP=2HPK
CALL SETPLOT(PTYP, 0, 0, 1)
XHI = 52.0
SCL = FLOAT(INT(SCL+0.5))
IF (SCL.GT.4.0) SCL = 4.0
IF (SCL.LT.1.0) SCL = 1.0
CALL PLOT(SCL, SCL, 0)
XHI = 52.0
PRINT 99996, NPTS1, NPTS2, SCL, VS, PCA, PCB, TSTEP, PTYP, NPRINT
READ (5,99998) A, B, PSCL
C NPTS1=NO. OF X VALUES,NPTS2=NO. OF T STEPS
C VP=P WAVE VELOCITY,VS=SHEAR W.V.,PCA,PCB ARE CONSTANTS
C DEFINING LOAD-TIME FUNCTION
READ (5,99997) (X(I),I=1,NPTS1)
VP = VS*(SORT(3.0))
WAVNP = 1.0/VP
WAVNS = 1.0/VS
WAVNR = 1.0/(0.9194*VS)
C CALCULATION OF CONSTANTS IN DISP. FUNCTION
CALL CON1(WAVNP, WAVNS, WAVNR, R, AA)
CALL CON2(WAVNP, WAVNS, WAVNR, R, BB)
CALL CON3(WAVNP, WAVNS, WAVNR, R, CC)
TIM(1) = 0.0
DO 10 I=2,NPTS2
TIM(I) = TIM(I-1) + TSTEP
10 CONTINUE
DO 30 K=1,NPTS1
R = X(K)
ENCODE(10,300,FRED)R
PRINT (6,99995) R
PRINT (6,99994)
DO 20 J=1,NPTS2
TPT = TIM(J)
RELACC = 1.0E-5
ABSACC = 0.0
IFAIL = 0
C INTEGRATION OF RAYLEIGH WAVE TERM
CALL D01ACF(A, B, FUN1, RELACC, ABSACC, ACC, ANS, NPTS,
*IFAIL)
SUMR(J) = ANS*0.282095/(PCA**3)
IF(NPRINT.EQ.1)PRINT(6,1600) ACC,NPTS
C INTEGRATION OF SHEAR WAVE TERM
CALL D01ACF(A, B, FUN2, RELACC, ABSACC, ACC, ANS, NPTS,
*IFAIL)
SUMS(J) = ANS*0.282095/(PCA**3)
IF(NPRINT.EQ.1)PRINT(6,1600) ACC,NPTS
C INTEGRATION OF P-WAVE TERM
CALL D01ACF(A, B, FUN3, RELACC, ABSACC, ACC, ANS, NPTS,

```

```

IFAIL)
SUMP(J) = ANS*0.282095/(PCA**3)
IF(NPRINT.EQ.1)PRINT(6,1600) ACC,NPTS
SUMT(J) = SUMR(J) + (SUMS(J) + SUMP(J))/PSCL
PRINT (6,99993) TIM(J), SUMR(J), SUMS(J), SUMP(J), SUMT(J)
20  CONTINUE
    CALL WPLT(SUMR, NPTS2, FRED, ITIT(1))
    CALL WPLT(SUMS, NPTS2, FRED, ITIT(2))
    CALL WPLT(SUMP, NPTS2, FRED, ITIT(3))
    CALL WPLT(SUMT, NPTS2, FRED, ITIT(4))
30  CONTINUE
    YHI = FLOAT(NPLOTS)/4.0
    YHI = YHI*SCL*13.0
    IF (PTYP.NE.2HZP) CALL DISPOZ(1, PTYP, XHI, YHI, 2HMS)
    STOP
99999 FORMAT (2I5, F5.0, 4F10.0, 3X, A2, I5)
99998 FORMAT (3F10.0)
99997 FORMAT (8F10.0)
300  FORMAT (F10.3)
99996 FORMAT (21H1CSIRO PROGRAM LLDISP, /, 21H -----, /,
*21H NO.OF X VALUES-----, I12, /, 21H NO.OF TIME STEPS-----, I12,
*/, 21H SCALE PARAMETER-----, F12.2, /, 21H SHEAR WAVE VELOCITY-,
*1PE12.4, /, 21H PCA-----, 1PE12.4, /, 12H PCB-----,
*9H-----, E12.4, /, 21H TIME STEP SIZE-----, E12.4, /,
*21H PLOTTER TYPE-----, 10X, A2, /, 21H PRINT-OUT PARAMETER-,
*I12)
99995 FORMAT (///, 1H, 131(1H-), /, 10X, 2HX=, F10.4, /, 1H, 131(1H-))
99994 FORMAT (15X, 9HTIME(SEC), 5X, 11HDISP.(RAYL), 8X, 12HDISP.(SHEAR),
*8X, 12HDISP.(COMP.), 8X, 12HDISP.(TOTAL))
1600  FORMAT (10X, 6HACC = , E11.4, 5X, 7HNPTS = , I3)
99993  FORMAT (10X, F10.5, 4(5X, 1PE15.8))
END
FUNCTION FUN1(OMEGA)
COMMON /PART1/ R, TPT, VP, VS, PCA, PCB, AA, BB, CC
WAVNR = OMEGA/(0.9194*VS)
THETA1 = OMEGA*(TPT-PCB)-WAVNR*R
CALL FTLF(OMEGA, PCA, FTL)
DPR = -AA*SIN(THETA1)
FUN1 = FTL*DPR
RETURN
END
FUNCTION FUN2(OMEGA)
COMMON /PART1/ R, TPT, VP, VS, PCA, PCB, AA, BB, CC
WAVNS = OMEGA/VS
THETA2 = OMEGA*(TPT-PCB)-WAVNS*R+ATAN(1.)
CALL FTLF(OMEGA, PCA, FTL)
BBN = BB/((R/VS)**1.5)
DPS = (BBN*SIN(THETA2))/(OMEGA**1.5)
FUN2 = FTL*DPS
RETURN
END
FUNCTION FUN3(OMEGA)
COMMON /PART1/ R, TPT, VP, VS, PCA, PCB, AA, BB, CC
WAVNP = OMEGA/VP
THETA3 = OMEGA*(TPT-PCB)-WAVNP*R+ATAN(1.)
CALL FTLF(OMEGA, PCA, FTL)
CCN = CC/((R/VP)**1.5)
DPP = (CCN*SIN(THETA3))/(OMEGA**1.5)
FUN3 = FTL*DPP
RETURN
END
SUBROUTINE WPLT(SUMX, NPTS2, FRED, ITITLE)

```



```

COMMON /PART2/ TIM(500), XLEN, NPLOTS, SCL
DIMENSION SUMX(500)
CALL AUTPLOT(TIM, SUMX, NPTS2, 1, 11H*TIME(SEC)*,
*14H*DISPLACEMENT*)
NPLOTS = NPLOTS + 1
CALL PLOT(3.5, 10.5, 3)
CALL TEXT(ITITLE, 9, 7)
CALL TEXT(FRED, 10, 7)
CALL PLOT(13.0, 13.0, 3)
CALL PLOT(0.0, 0.0, 1)
XLEN = XLEN + 13.0
X = 52.0/SCL
IF (XLEN.LT.X) GO TO 10
CALL PLOT(-14.0, -X, 3)
XLEN = 0.0
CALL PLOT(0.0, 0.0, 1)
10 CONTINUE
RETURN
END
SUBROUTINE CON1(W1, W2, W3, R, AA)
BETA1 = (W3**2) - (W1**2)
BETA2 = (W3**2) - (W2**2)
DELRF1 = 2*(W3**2) - W2**2
DELRF2 = SQRT(BETA1*BETA2)
DELRF3 = 0.5*(W3**2)*(SQRT(BETA2/BETA1))
DELRF4 = 0.5*(W3**2)*(SQRT(BETA1/BETA2))
DELRF = (8*W3)*(DELRF1-DELRF2-DELRF3-DELRF4)
AA = -(W2**2)*(SQRT(BETA1))/(DELRF)
RETURN
END
SUBROUTINE CON2(W1, W2, W3, X, BB)
BB = 1.0 - (W1**2)/(W2**2)
BB = 1.59577*BB
RETURN
END
SUBROUTINE CON3(W1, W2, W3, X, CC)
CC = (W1*W2)**2
CC = CC/(((W2**2)-2*(W1**2))**2)
CC = 0.39894*CC
RETURN
END
SUBROUTINE DISPOZ(LUN, PTYP, XSIZE, YSIZE, ST)
DIMENSION ID(3)
C
C THIS ROUTINE CALL SYSTEM ROUTINE DISPOSE TO
C DISPOSE THE PLOT ON FILE LUNTO THE NETWORKWITH THE
C SIZE IN CM. SPECIFIED IN THE 'FID' PARAMETER
C ALL PARAMETERS NEED TO BE IN L FORMAT(LEFT JUSTIFIED ZERO FILLED)
C THE COLON (:) IS THE CHARACTER CODE FOR ZERO
IX = INT(XSIZE)
IY = INT(YSIZE)
PRINT 99999, IX, IY
CALL JOBID(ID)
ENCODE(10,1,STAT)ST
ENCODE(10,2,ATYP)PTYP
ENCODE(10,3,FID)ID(2),IX,IY
CALL DISPOSE(LUN, STAT, ATYP, 0, FID)
CALL PLOCHOP(1)
CALL REMARK(19H PLOT FILE DISPOSED)
RETURN
1 FORMAT (3HR10, A2, 5H:::~)
2 FORMAT (1H*, A2, 7H:::~)

```

```
3 FORMAT (A1, I2, 1H*, I3, 3H:::)  
99999 FORMAT (///, 10X, 24H PLOT DIMENSIONS WILL BE, 15, 6H CM BY, 15,  
*3H CM)  
END  
SUBROUTINE FTLF(OMEGA, PCA, FTL)  
C FOURIER TRANSFORM OF LOAD TIME FUNCTION  
FTL = EXP(-3.*((OMEGA/(2.0*PCA))**2))  
FTL = -(OMEGA**3)*FTL  
RETURN  
END
```

Appendix 2. Relevant publications by the author

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Telephone: (03) 266 3601 Telex: AA151143 SEP MEL Fax: (03) 267 4051.

TW2506/AU
PK/PK

May 27, 1987

The Chief
CSIRO
Division of Geomechanics
PO Box 54
MOUNT WAVERLY Vic 3149

ATTENTION: Mr G.G. Shorten

Dear Sir

Australian Provisional Patent Application No PI1967/87
COMMONWEALTH SCIENTIFIC AND INDUSTRIAL RESEARCH ORGANISATION
"FORCE TRANSDUCER"

We are pleased to report that the abovementioned application was lodged in the Australian Patent Office on 18 May 1987 and was allocated the number PI1967/87.

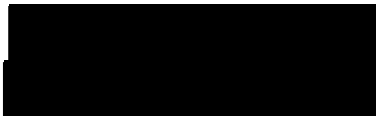
As you may be aware, it is essential that any applicant(s) for the grant of Letters Patent have a clear title to the invention from the actual inventor(s).

We enclose (in duplicate) an acknowledgement that the invention, the subject of this patent application, is the property of the CSIRO.

Would you please arrange for each inventor to insert his full name, nationality and complete residential address, and to execute the acknowledgements in the presence of a witness.

Please return one of the executed acknowledgements to Sirotech Limited at your earliest convenience. The second acknowledgement can be retained for your file.

Yours faithfully



Paul Kilborn
CORPORATE PATENT ATTORNEY
Intellectual Property Group

encl.:

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FOR	FILE
DATE	
A/Chief	29/5
GGS	J
L Hunt	4/6
A. Shorten	7/6
GGS	2/6
GGS	5/6
TWI/111/9	

X

TW2506/AU

IN THE MATTER OF an invention entitled:

"FORCE TRANSDUCER"

as described in the specification of Australian Patent Application
No: PI1967/87

We*/I (Insert full name of each Inventor)

LEIGH DAVID HUNT
ANTHONY FREDERICK SIGGINS

Citizen(s*) of (Insert Nationality of each Inventor)

AUSTRALIAN

AUSTRALIAN, respectively*

of (Insert full residential address of each Inventor)

3 BARBER CRT CHELTENHAM
VICTORIA

38 MYERS AVE SLEN WAVERLEY
VICTORIA 3150, respectively*

HEREBY ACKNOWLEDGE AND DECLARE that the above invention was made by
~~me~~/us* in the course of ~~my~~/our* official duties with the
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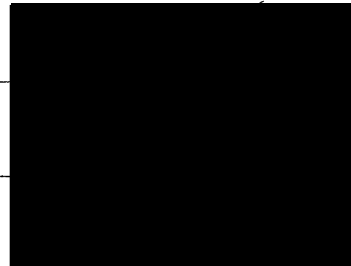
L. D. Hunt

Witness:

A. F. Siggins

Witness:

* Delete where appropriate



**Circumferential propagation of elastic waves on boreholes
and cylindrical cavities**

A. F. Siggins and A. N. Stokes

GEOPHYSICS, VOL. 52, NO. 4 (APRIL 1987); P. 514-529, 15 FIGS., 2 TABLES.